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# Rheozama project: slurry casting application to hot chamber zinc die casting

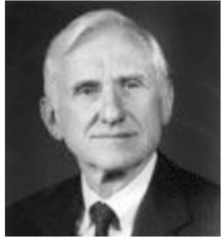
Tommaso Botter, Mambretti Tech (Italy)

September 11<sup>th</sup>, 2025

Zinc Die Casting Conference 2025



# Introduction to Slurry Casting



*Materials Science and Engineering*, 25 (1976) 103 - 117  
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## Rheocasting

It has been discovered recently, however, that when metal alloys are vigorously agitated during solidification, the solid which forms has a special “non-dendritic” structure [3 - 5]. Partially-solidified metals with this special structure behave as highly fluid slurries at fractions solid as high as 0.60. They can be



Liquid



Superheated Slurry



Slurry



Semi-solid



# Gas Induced Superheated Slurry



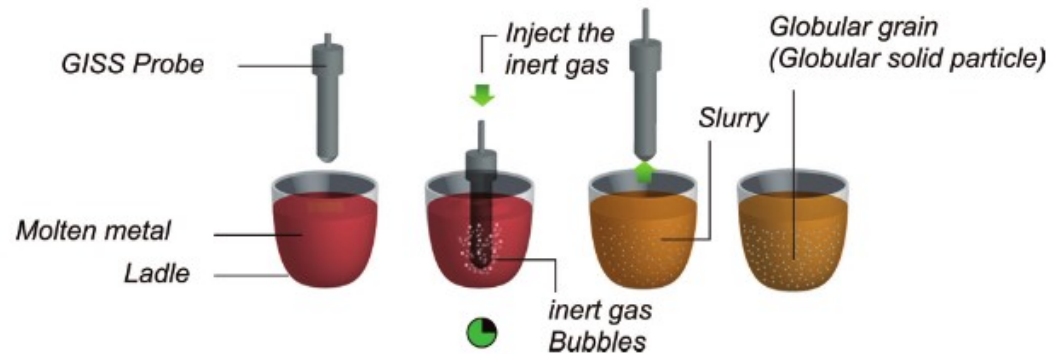
The process can be divided into four steps:

Step 1: **Placing a probe into the melt** to remove a controlled amount of heat.

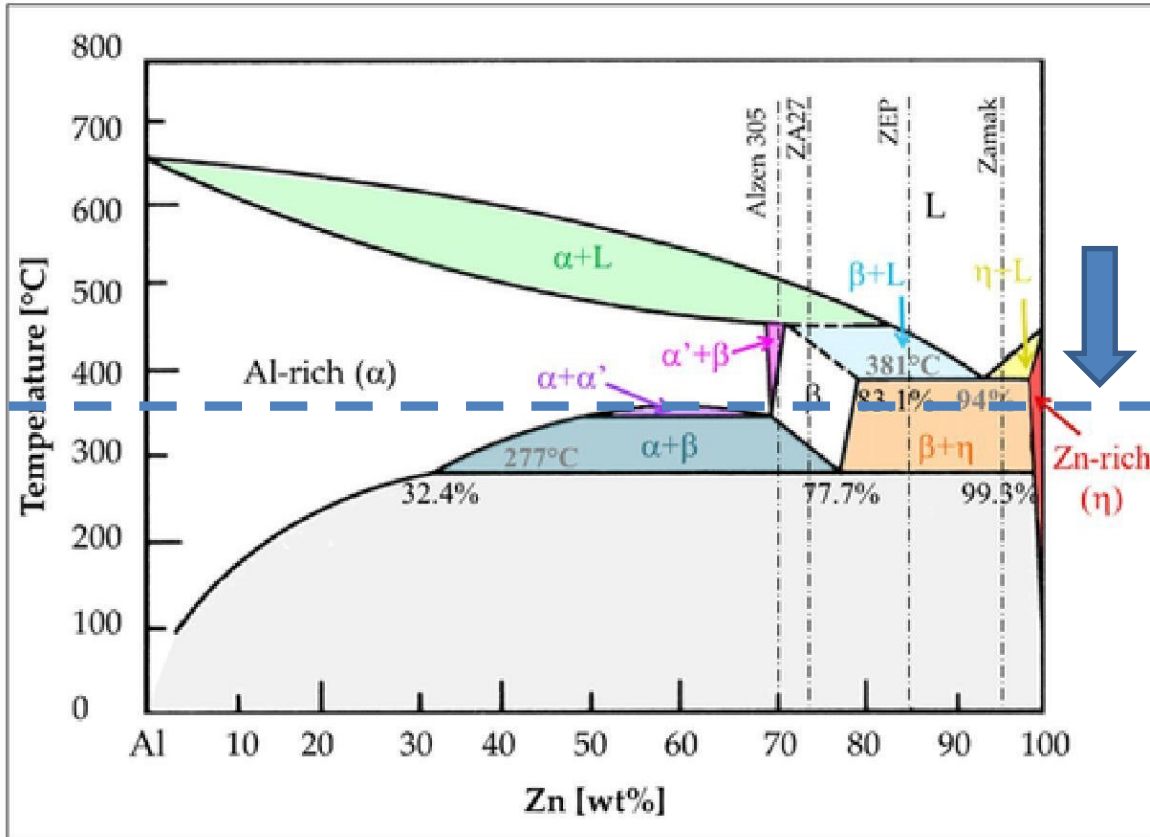
Step 2: **Vigorous convection** by injection of inert gas bubbles is applied to the melt to assure nearly uniform cooling of the melt to the temperature slightly above the liquidus temperature and also to create solid nuclei.

Step 3. The probe is then rapidly removed from the melt when the desired **solid fraction** is reached.

Step 4: The melt is quickly transferred to a mold for casting into parts.



# Gas Induced Superheated Slurry



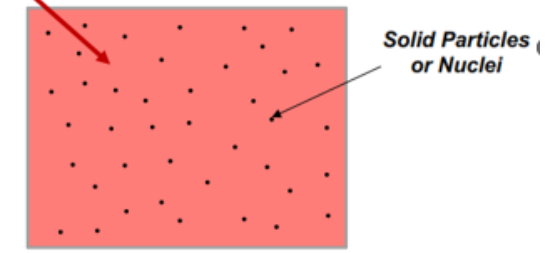
$T_{\text{semi-solid}}$  is in  $T_L$  and  $T_S$  range

$T_L > \text{Al} > T_S \approx 60^\circ\text{-}70^\circ$

$T_L > \text{ZA5} > T_S \approx 6\text{-}8^\circ$

$T_{\text{slurry}} > T_L$

**$T_{\text{GISS}}$  is above  $T_L$**



# Gas Induced Superheated Slurry



Through GISS technology, a small fraction of fine solid nuclei is created in the melt even though the bulk liquid melt is at the temperature **slightly above the liquidus temperature.**

## Applicability:

- No need to change gate size
- No need to modify runners
- Any alloy
- Rapid installation time
- Movable to any convenient DCM

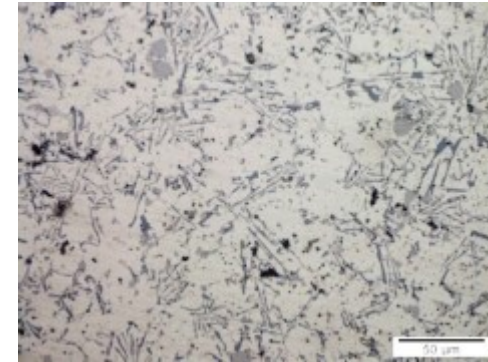
The **fraction of solid** changes the flow pattern into the die cavity. As a result, gas porosity can be effectively controlled. Furthermore, the presence of **pre-existing solid particles** in the slurry changes the solidification mode of the metal in the die cavity such that shrinkage porosity is greatly reduced.

# Key features – cold chamber

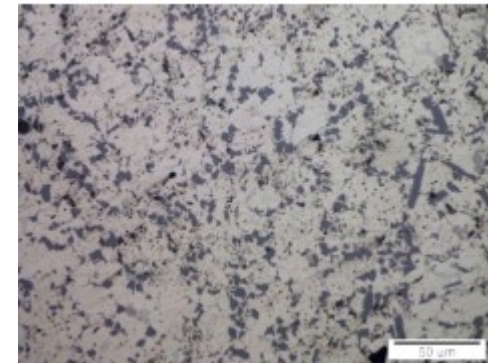


- Gas porosity is reduced in the GISS casting process because the controlled solid fraction in the slurry implies **less turbulent flow** compared with conventional high-pressure die casting.
- Shrinkage porosity is reduced in the GISS casting process because the initial solid particles present in the slurry act as nucleation sites in liquid metal. Additionally, the temperature range from metal temperature in the cavity and the solidification temperature is lower, consequently the solidification time is shorter, and the shrinkage porosities decrease.
- Slurries enter the die with significantly **reduced heat content**, resulting in shorter cycle time and longer die life.
- Solid particles in the slurries are ultra-fine, yielding easy flow into the ultra-thin sections and uniform microstructure.

Comparison of microstructure of alloy A383 (AlSi11Cu3)



Conventional HPDC



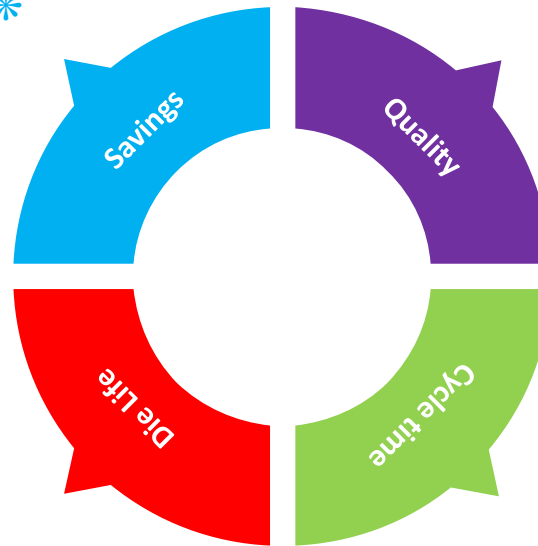
GISS Technology

# Key benefits (cold chamber)



Energy Savings (Furnace) \*  
Water treatment reduction \*  
Ev. DCM Size reduction \*

Gas Porosity \*  
Shrinkage Porosity \*  
Planarity \*



Min Die Temperature \*  
Less Time of cast Part into the  
mould \*  
Less Lubricant Quantity per Shot \*

Min Solidification Time \*  
Min Lubrication-Blowing Time \*  
Faster Slow Phase \*



## Mini slurry casting project

- ZA3 alloy
- Cold chamber vertical machine
- Machine tonnage 5t
- Temperature  $\approx 5^\circ > T_{liq}$
- $\rightarrow$  Vertical Slurry Casting

## Structure and properties of stir-cast zinc alloys

H LeHuy, J Blain, J Masounave, GL Bata

TMS (The Metallurgical Society) Paper Selection;(USA), 1984 - [osti.gov](http://osti.gov)

Stir casting (or rheocasting) of ZA-27 zinc alloys was investigated experimentally. By vigorously agitating the alloys during cooling, the dendrites that were forming were fragmented giving a unique structure composed of spherical and rosette shaped particles

## Forming Gears from ZA-27 Zinc Alloy Using Semi-Solid Slurry Squeeze Casting Process

**Thawatchai Plookphol, Somjai Janudom, Supakit Vongcharoenpon**

Department of Mining and Materials Engineering, Faculty of Engineering  
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[thawatchai.p@psu.ac.th](mailto:thawatchai.p@psu.ac.th); [somjai.ja@psu.ac.th](mailto:somjai.ja@psu.ac.th); [supakit.vong@gmail.com](mailto:supakit.vong@gmail.com)

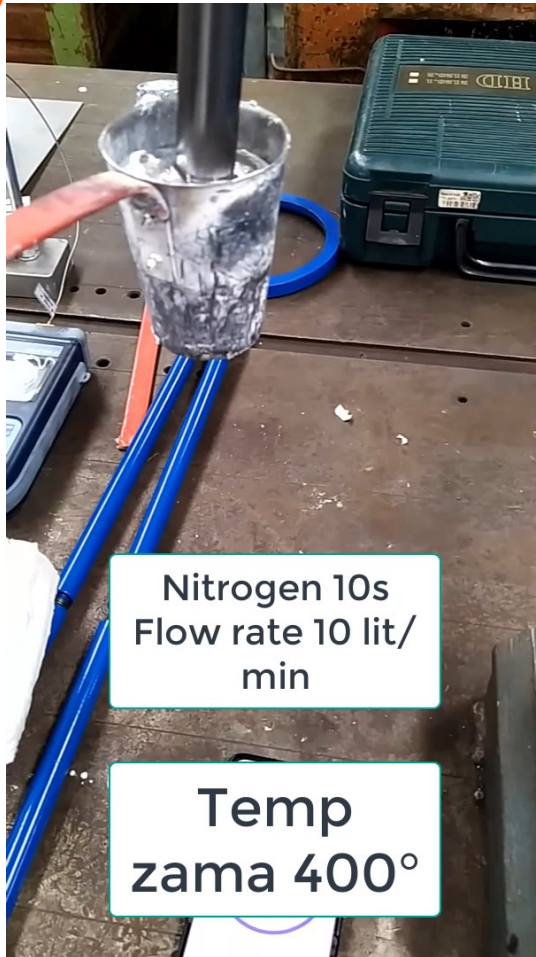
## Aluminum segregation in ZA27 rheocast alloy

Annalisa Pola<sup>1, a</sup>, Lorenzo Montesano<sup>1, b</sup>, Marcello Gelfi<sup>1, c</sup>, Roberto Roberti<sup>1, d</sup>  
and Giovina Marina La Vecchia<sup>1, e</sup>

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<sup>d</sup> [roberto.roberti@ing.unibs.it](mailto:roberto.roberti@ing.unibs.it), <sup>e</sup> [marina.lavecchia@ing.unibs.it](mailto:marina.lavecchia@ing.unibs.it)

# Slurry Test



# Castle Rheo Simulation Software



3D MESH RHEO FILLING RHEO SOLIDIFICATION

**PROJECT FOLDER** C:\Users\AndreaP\Desktop\A\_RHEO LOAD SIMULATION

**SIMULATION DATA**  
 Simulation name: FillingRHEO\_HC CC  3P LOAD MESH C:\Users\AndreaP\Desktop\A\_RHEO\BodyMeshHC\BodyMeshHC\_Mesh VIEW MESH Gravity di: -x

**SHOT SLEEVE MODELING**  Standard  Plunger Motion

**INJECTION PROFILE**  Standard  Custom EDIT

**OTHER OPTIONS**  Solidification SELECT PROBES LOAD PARAMETERS

**PROCESS PARAMETERS**  
 Alloy: ? ZN\_Zamak5\_ZL5\_ZA410\_GISS  
 Treatment Time [s]: 2  
 Treatment Temperature [°C]: 405  
 Pouring delay Time [s]: 1  
 Tool steel: W1.2343 H11 ZN HC  
 Die temperature [°C]: 120  
 Fast shot Static Pressure [bar]: 300  
 Venting:  Standard  Advanced EDIT

**POST TREATMENT CONDITIONS**  
 Initial solid fraction: 2.8 Final solid fraction: 7.7 Alloy temperature [°C]: 402

**INJECTION PARAMETERS**  
 Total volume [cm³]: 7.722 Slow shot speed [m/s]: 0.54 Nozzle diameter [mm]: 5.89 Slow shot time [s]: 0.0048  
 Fast shot volume [cm³]: 5.000 Fast shot speed [m/s]: 0.60 Nozzle Speed 2 [m/s]: 42.87 Acceleration time [s]: 0.0002  
 Fast shot start: 60.1 Fast shot time [s]: 0.0089  
 Stroke shift [mm]=0:  Prefilling ratio: 0%  
 -2.72 5.09 Filling Mode: Standard  
 Nozzle Speed 1 [m/s]: 60.1  
 Alloy at gates [mm]: 60.22  
 Complete filling [mm]: 65.31

**SHOT SLEEVE**  
 Plunger Diameter [mm]: 50.00  
 Prestroke [mm]: 57.50

**SIMULATION PARAMETERS**  
 Slow shot: write interval: 0.0005 SS Frames: 10 Simulation backup:  Compressed backu:   
 Fast shot: write interval: 0.0005 FS Frames: 18 Destination backup:   
 Number of processors: 6 Insert note: FillingRHEO\_HC COMMENT  
 Calculation speed: 1,0  
 0,2 1,3

SyMO RUN PAUSE RESTART STOP FAST SHOT VIEW QUEUE VIEW LOG

0%

# Castle Rheo Simulation Software



**PROCESS PARAMETERS**

Alloy ? ZN\_Zamak5\_ZL5\_ZA410\_GISS

Treatment Time [s] 5

Treatment Temperature [°C] 405

Pouring delay Time [s] 1

Tool steel W1.2343 H11 ZN HC

Die temperature [°C] 120

Final Holding Pressure [bar] 300

Venting

**INFO**

Liquidus temperature [°C] 386

Solidus temperature [°C] 380

Alloy Liquidus and Solidus Temperature

GISS Time: number of seconds the probe is in the melt

Metal temperature when the probe is in the melt

Calculated solid fraction immediately after application

**POST TREATMENT CONDITIONS**

Initial solid fraction 2.8 Final solid fraction 7.7 to

# Rheozama project



Furnace Temp 400°  
Probe Dip Time 10s  
Probe Temp 40°

Crucible with movable bulkheads to limit the amount of metal being treated

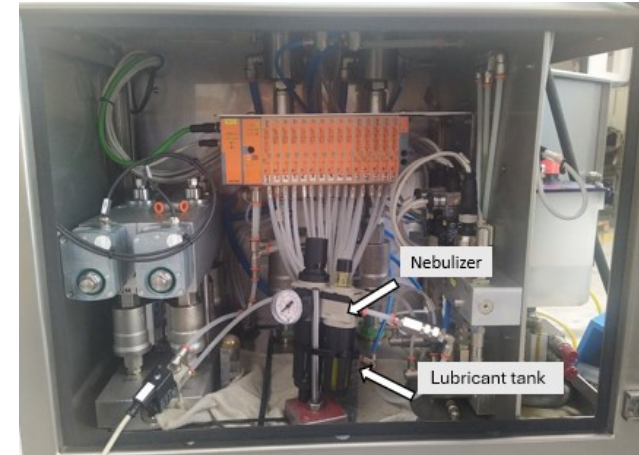
# Rheozama project



ZL5 - ZnAl4Cu1

Rheo Time 5s  
Subdivided crucible

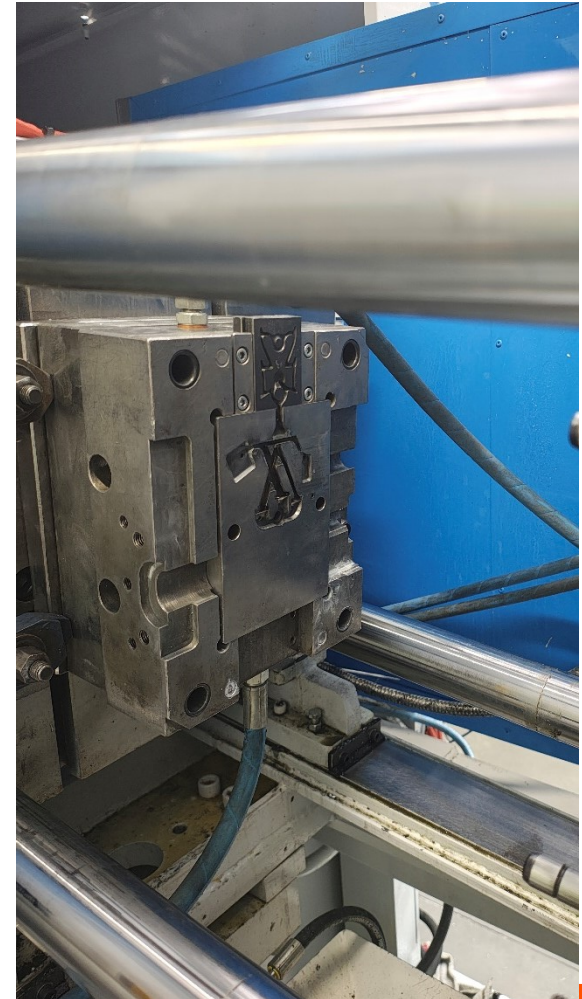
Integration of vacuum technology to convey a lubricant modified in its state from liquid to aerosol (or oily mist) and then conveyed inside the die through the vacuum suction valve.



# Rheozama project



Application to a production mold. Cycle time about 20s, dip time 15s not related to cycle



# Rheozama project



Furnace Temp  $\approx 405^\circ$

⚠  $< 400^\circ$



Probe Temp  $\approx 45C$

⚠  $> 90^\circ$



6 bar @ 20 ml/min

⚠  $< 5$  bar

# Castle Rheo Simulation Software



Time: 0.000300

Dual phase

Liquid



Time: 0.000400

GISS



# Castle Rheo Simulation Software



Time: 0.000300

Liquid

Speed



Time: 0.000400

GISS



# Castle Rheo Simulation Software



Time: 0.000300

Liquid



Liquid

Air 30%

Time: 0.000400

GISS



Rheo

# Castle Rheo Simulation Software



Gas Porosity 1%

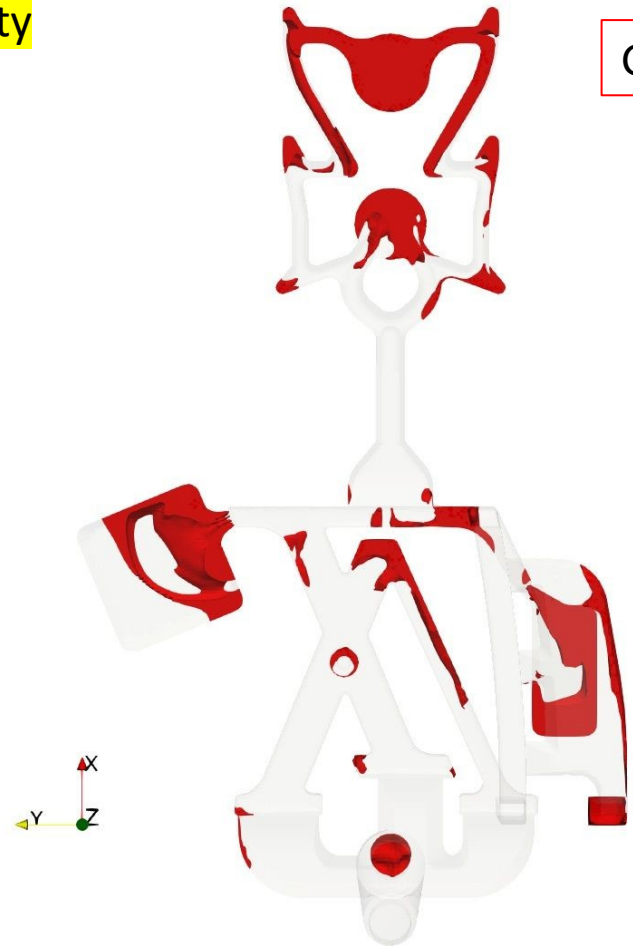
Liquid



Gas Porosity

Gas Porosity 1%

GISS



# Castle Rheo Simulation Software



Gas Porosity 5%

Liquid



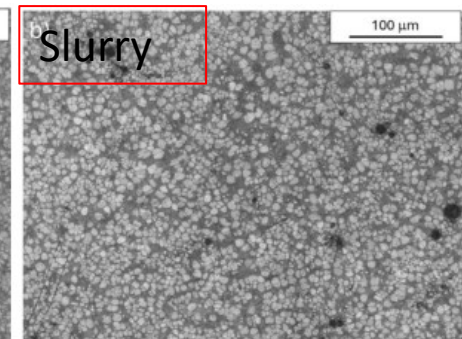
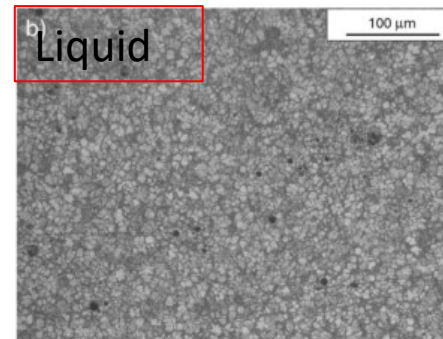
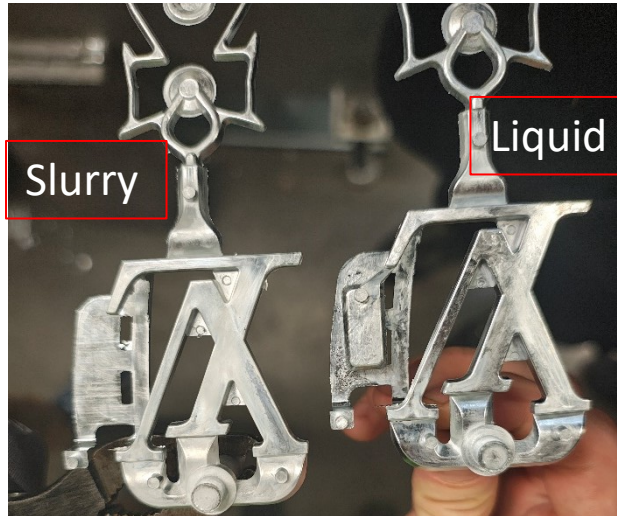
Gas Porosity

Gas Porosity 5%

GISS



# Rheozama project

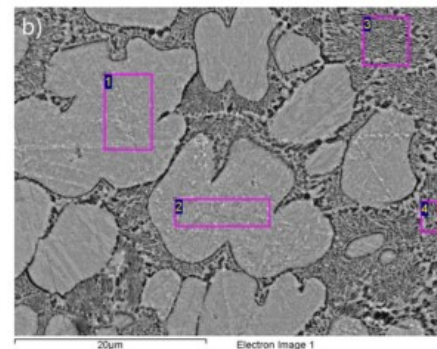


Liquid: primary phase pseudo dendritic

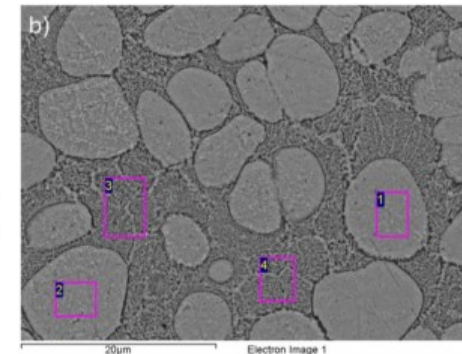
Slurry: more globular shape

	No slurry U-B	Slurry U-G
Densità Media [gr/cm <sup>3</sup> ]	6.630	6.640
dev. Std.	0.046	0.019
Porosità %	0.3	0.15

Tabella I Risultati misure di densità



Spectrum	O wt.%	Al wt.%	Cu wt.%	Zn wt.%
1	5.58	2.09	2.47	89.85
2	6.00	2.00	2.85	89.14
3	6.93	10.82	1.99	80.26
4	6.92	11.42	2.44	79.22



Spectrum	O wt.%	Al wt.%	Cu wt.%	Zn wt.%
1	2.51	2.46	2.66	92.37
2	3.15	2.42	2.51	91.91
3	3.53	11.27	2.02	83.18
4	3.19	11.30	2.97	82.55



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## Summary

The Rheozama Project aimed to investigate the possibility of applying slurry technology to traditional hot chamber die casting, using a standard zinc alloy and without modifying the mold. So far, the application of the technology had been limited by some peculiar aspects of HCDC:

- the very small liquidus-solidus temperature range
- the difficulty of limiting the amount of metal where the slurry is formed
- the reduced benefits of the hot chamber compared to the cold chamber

The project has tried to go beyond these limitations through:

- ✓ The adoption of GISS technology that works at  $T_{\text{slurry}} > T_{\text{liq}}$
- ✓ DCM crucible modifications
- ✓ The introduction of a closed-mould lubrication system through the vacuum valve
- ✓ Development of an ad hoc software simulator to verify the potential benefits in advance



The results confirmed the possibility of generating slurry for zinc alloys but also the difficulty of applying it to the standard process without further modifications of DCM.

Experience has highlighted some critical issues, in particular the need to further limit the amount of metal to be treated and to cool the probe more. The changes will be prepared in the coming months and will be the subject of further studies.

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